CHAPTER13

Three-Phase Circuits

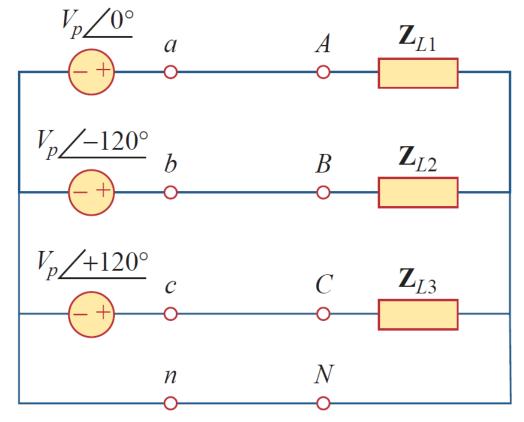
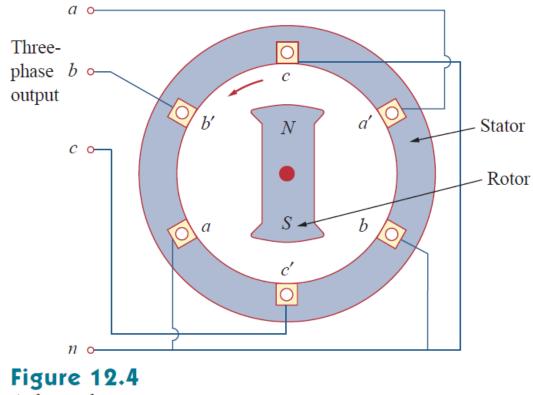


Figure 12.3 Three-phase four-wire system.

- Three-phase systems are important for at least three reasons.
- First, nearly all electric power is generated and distributed in three-phase.
- Second, the instantaneous power in a threephase system can be constant (not pulsating), This results in uniform power transmission and less vibration of three-phase machines.
- Third, for the same amount of power, the threephase system is more economical than the single phase.The amount of wire required for a threephase system is less than that required for an equivalent single-phase system.

12.2 Balanced Three-Phase Voltages

Three-phase voltages are often produced with a three-phase ac generator (or alternator) whose cross-sectional view is shown in Fig. 12.4. The generator basically consists of a rotating magnet (called the *rotor*) surrounded by a stationary winding (called the *stator*). Three separate



A three-phase generator.

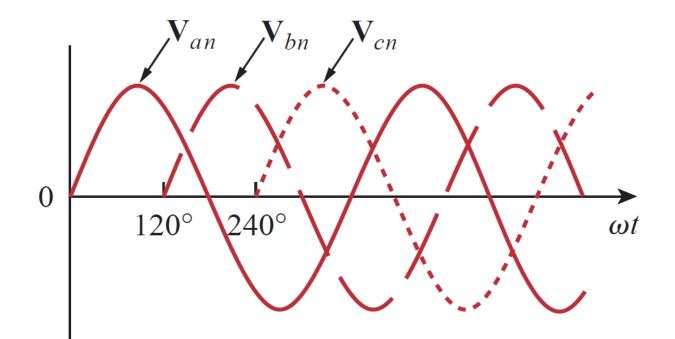


Figure 12.5

The generated voltages are 120° apart from each other.

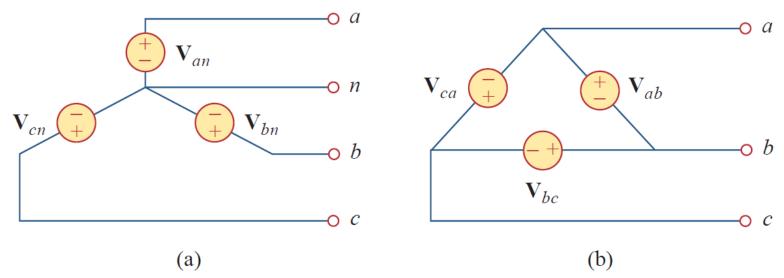
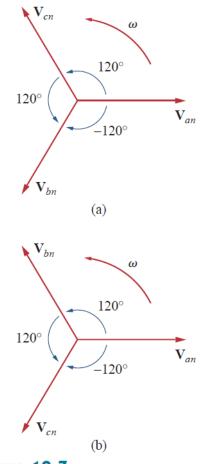


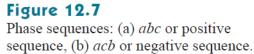
Figure 12.6

Three-phase voltage sources: (a) Y-connected source, (b) Δ -connected source.

Balanced phase voltages are equal in magnitude and are out of phase with each other by 120°.



$$\mathbf{V}_{an} + \mathbf{V}_{bn} + \mathbf{V}_{cn} = 0$$
$$|\mathbf{V}_{an}| = |\mathbf{V}_{bn}| = |\mathbf{V}_{cn}|$$



where V_p is the effective or rms value of the phase voltages. This is known as the *abc sequence* or *positive sequence*. In this phase sequence, V_{an} leads V_{bn} , which in turn leads V_{cn} . This sequence is produced when the rotor in Fig. 12.4 rotates counterclockwise. The other possibility is shown in Fig. 12.7(b) and is given by

$$\mathbf{V}_{an} = V_p / \underline{0^{\circ}}$$

$$\mathbf{V}_{cn} = V_p / \underline{-120^{\circ}}$$

$$\mathbf{V}_{bn} = V_p / \underline{-240^{\circ}} = V_p / \underline{+120^{\circ}}$$

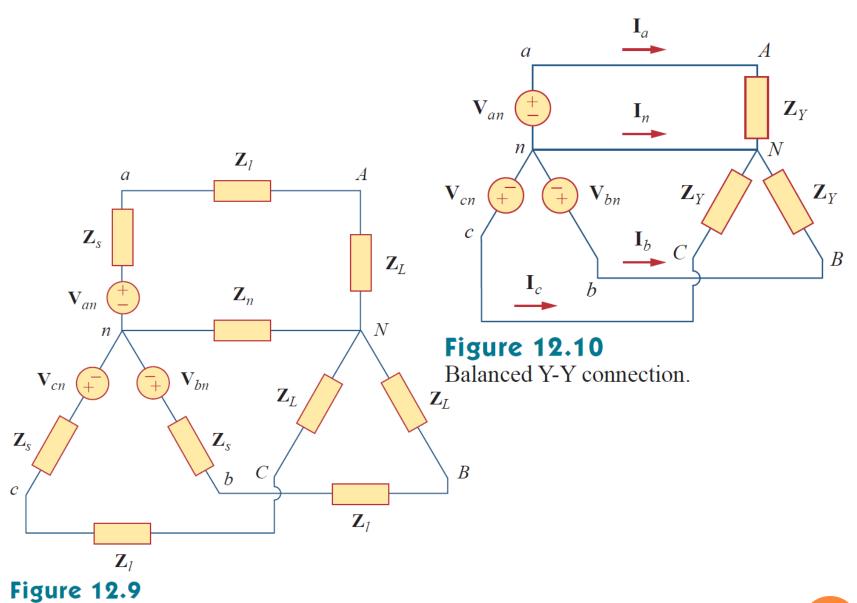
(12.4)

$$\mathbf{V}_{an} + \mathbf{V}_{bn} + \mathbf{V}_{cn} = V_p / \underline{0^{\circ}} + V_p / \underline{-120^{\circ}} + V_p / \underline{+120^{\circ}}$$
$$= V_p (1.0 - 0.5 - j0.866 - 0.5 + j0.866)$$
$$= 0$$

A **balanced load** is one in which the phase impedances are equal in magnitude and in phase.

Reminder: A Y-connected load consists of three impedances connected to a neutral node, while a Δ -connected load consists of three impedances connected around a loop. The load is balanced when the three impedances are equal in either case.

 $Z_{1} = Z_{2} = Z_{3} = Z_{Y}$ $Z_{a} = Z_{b} = Z_{c} = Z_{\Delta}$ $Z_{\Delta} = 3Z_{Y} \quad \text{or} \quad Z_{Y} = \frac{1}{3}Z_{\Delta}$



A balanced Y-Y system, showing the source, line, and load impedances.

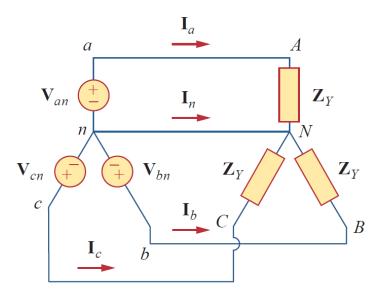
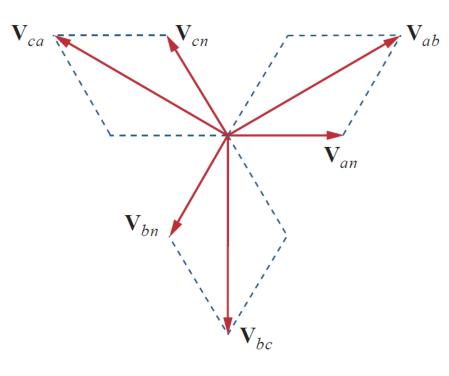


Figure 12.10 Balanced Y-Y connection.



(b)

Figure 12.11

Phasor diagrams illustrating the relationship between line voltages and phase voltages.

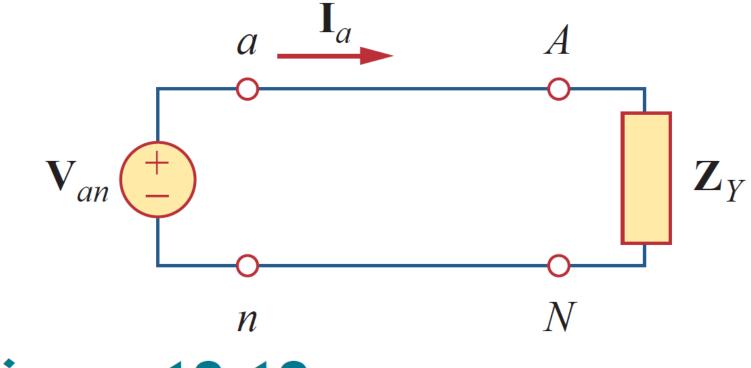


Figure 12.12 A single-phase equivalent circuit.

Calculate the line currents in the three-wire Y-Y system of Fig. 12.13.

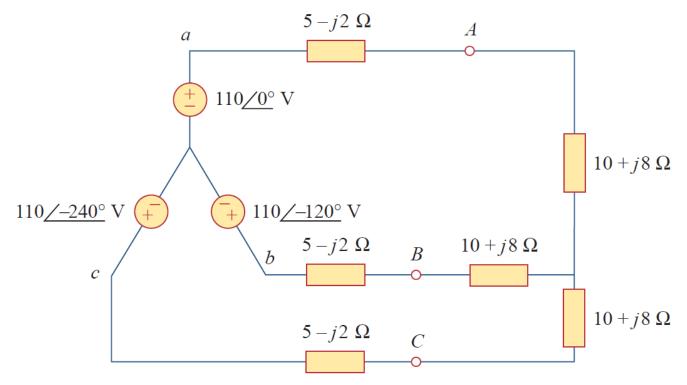


Figure 12.13 Three-wire Y-Y system; for Example 12.2.

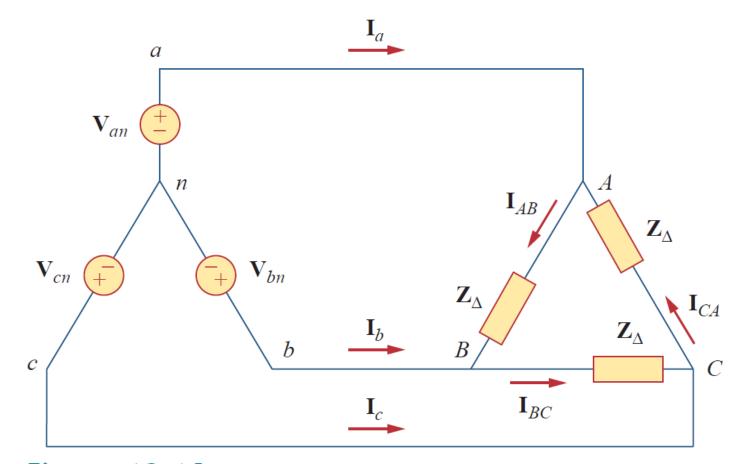


Figure 12.14 Balanced Y- Δ connection.

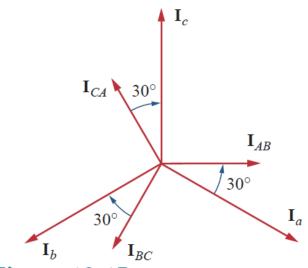


Figure 12.15

Phasor diagram illustrating the relationship between phase and line currents.

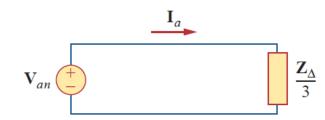


Figure 12.16

A single-phase equivalent circuit of a balanced Y- Δ circuit.

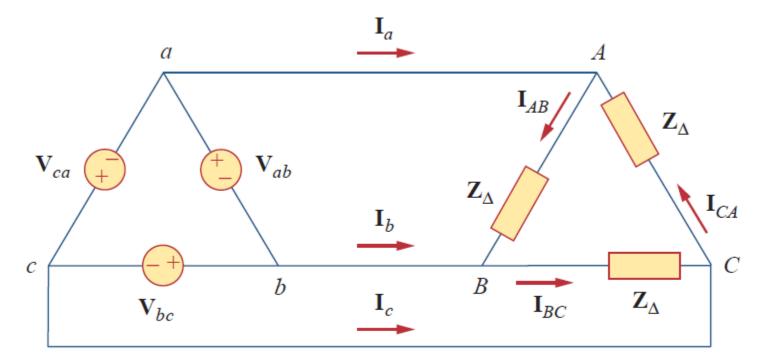


Figure 12.17 A balanced Δ - Δ connection.

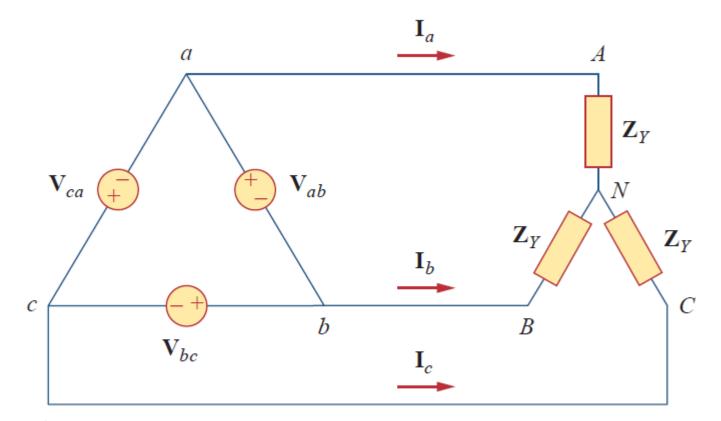


Figure 12.18 A balanced Δ -Y connection.

12.15 The circuit in Fig. 12.48 is excited by a balanced three-phase source with a line voltage of 210 V. If **DS** $\mathbf{Z}_I = 1 + j1 \ \Omega, \mathbf{Z}_{\Delta} = 24 - j30 \ \Omega$, and $\mathbf{Z}_Y = 12 + j5 \ \Omega$, determine the magnitude of the line current of the combined loads.

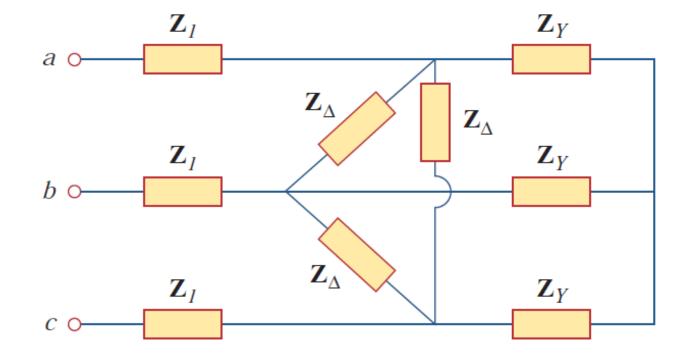
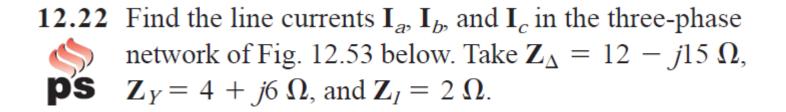


Figure 12.48 For Prob. 12.15.



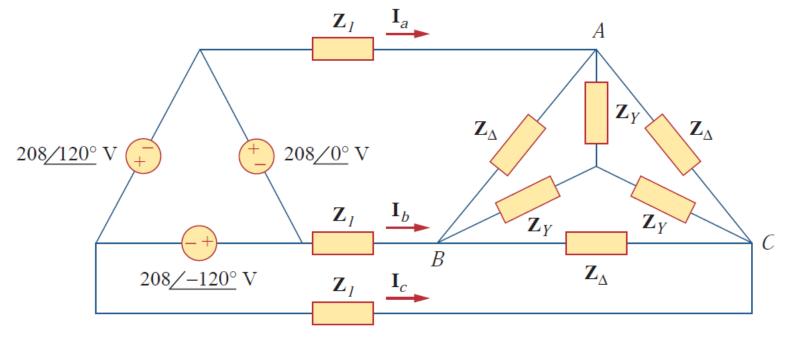
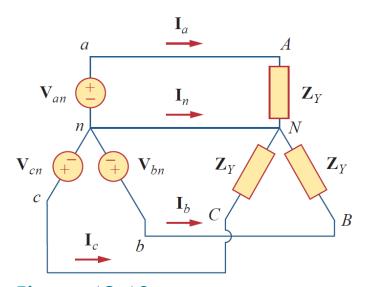


Figure 12.53 For Prob. 12.22.

POWER IN A BALANCED SYSTEM $v_{AN} = \sqrt{2} V_p \cos \omega t, \quad v_{BN} = \sqrt{2} V_p \cos(\omega t - 120^\circ)$ $v_{CN} = \sqrt{2} V_p \cos(\omega t + 120^\circ)$ $i_a = \sqrt{2} I_p \cos(\omega t - \theta), \quad i_b = \sqrt{2} I_p \cos(\omega t - \theta - 120^\circ)$ $i_c = \sqrt{2} I_p \cos(\omega t - \theta + 120^\circ)$



For balanced system, current in neutral line is zero. The neutral line existing or not will have the same result.

Figure 12.10 Balanced Y-Y connection.

$$p = p_a + p_b + p_c = v_{AN}i_a + v_{BN}i_b + v_{CN}i_c$$

= $2V_p I_p [\cos \omega t \cos(\omega t - \theta) + \cos(\omega t - 120^\circ) \cos(\omega t - \theta - 120^\circ) + \cos(\omega t + 120^\circ) \cos(\omega t - \theta + 120^\circ)]$ (12.43)

Applying the trigonometric identity

$$\cos A \cos B = \frac{1}{2} [\cos(A + B) + \cos(A - B)]$$
 (12.44)

gives

$$p = V_p I_p [3 \cos \theta + \cos(2\omega t - \theta) + \cos(2\omega t - \theta - 240^\circ) + \cos(2\omega t - \theta + 240^\circ)]$$

$$= V_p I_p [3 \cos \theta + \cos \alpha + \cos \alpha \cos 240^\circ + \sin \alpha \sin 240^\circ + \cos \alpha \cos 240^\circ - \sin \alpha \sin 240^\circ] \qquad (12.45)$$
where $\alpha = 2\omega t - \theta$

$$= V_p I_p \left[3 \cos \theta + \cos \alpha + 2\left(-\frac{1}{2}\right) \cos \alpha \right] = 3 V_p I_p \cos \theta$$

$$P_p = V_p I_p \cos\theta \tag{12.46}$$

and the reactive power per phase is

$$Q_p = V_p I_p \sin\theta \tag{12.47}$$

The apparent power per phase is

$$S_p = V_p I_p \tag{12.48}$$

The complex power per phase is

$$\mathbf{S}_p = P_p + jQ_p = \mathbf{V}_p \mathbf{I}_p^* \tag{12.49}$$

where V_p and I_p are the phase voltage and phase current with magnitudes V_p and I_p , respectively. The total average power is the sum of the average powers in the phases:

$$P = P_a + P_b + P_c = 3P_p = 3V_p I_p \cos\theta = \sqrt{3}V_L I_L \cos\theta \quad (12.50)$$

UNBALANCED THREE-PHASE SYSTEMS

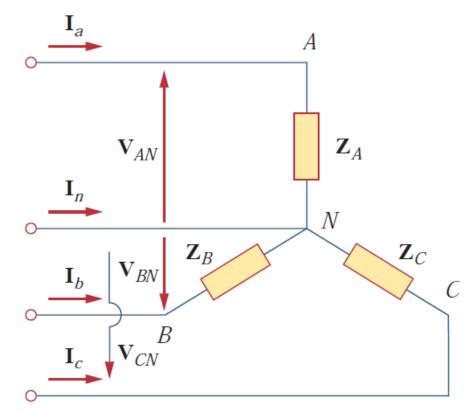


Figure 12.23

Unbalanced three-phase Y-connected load.

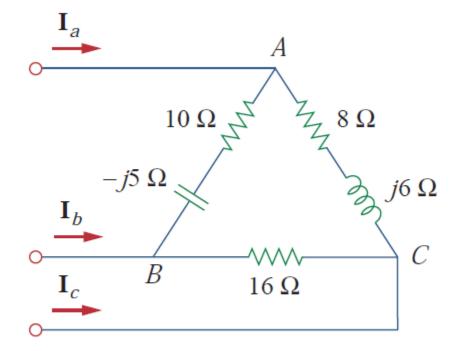
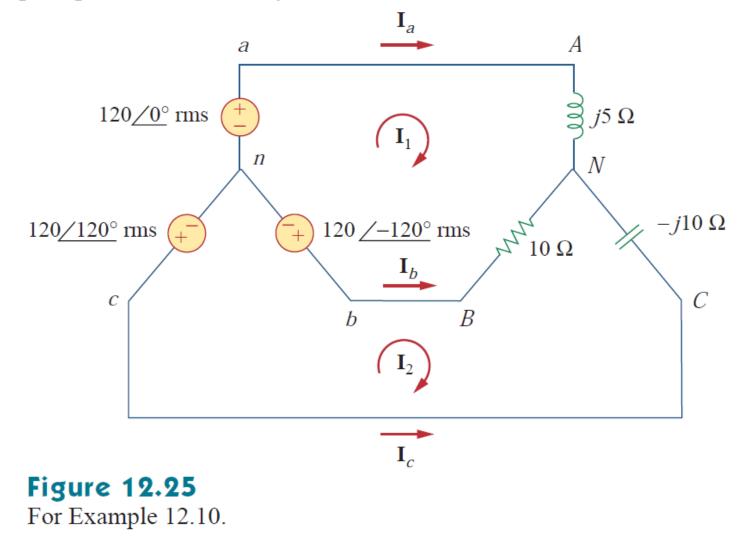


Figure 12.24 Unbalanced Δ -load; for Practice Prob. 12.9.

For the unbalanced circuit in Fig. 12.25, find: (a) the line currents, (b) the total complex power absorbed by the load, and (c) the total complex power absorbed by the source.



POWER MEASURMENT

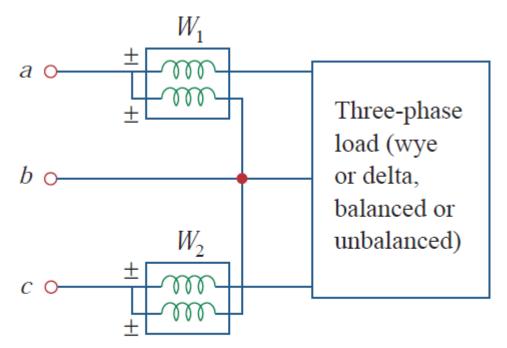


Figure 12.34

Two-wattmeter method for measuring three-phase power.

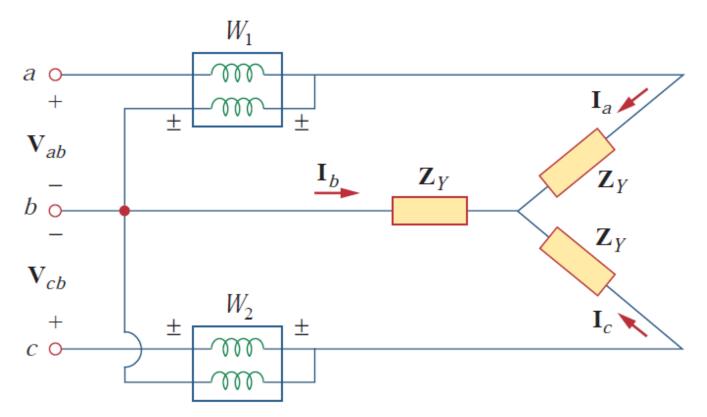


Figure 12.35

Two-wattmeter method applied to a balanced wye load.

 $P_1 = \operatorname{Re}[\mathbf{V}_{ab}\mathbf{I}_a^*] = V_{ab}I_a\cos(\theta + 30^\circ) = V_LI_L\cos(\theta + 30^\circ)$ $P_2 = \operatorname{Re}[\mathbf{V}_{cb}\mathbf{I}_c^*] = V_{cb}I_c\cos(\theta - 30^\circ) = V_LI_L\cos(\theta - 30^\circ)$

 $P_1 + P_2 = V_L I_L [\cos(\theta + 30^\circ) + \cos(\theta - 30^\circ)]$ = $V_L I_L (\cos\theta \cos 30^\circ - \sin\theta \sin 30^\circ)$ + $\cos\theta \cos 30^\circ + \sin\theta \sin 30^\circ)$ = $V_L I_L 2 \cos 30^\circ \cos\theta = \sqrt{3} V_L I_L \cos\theta$

$$P_T = P_1 + P_2$$

$$P_{1} - P_{2} = V_{L} I_{L} [\cos(\theta + 30^{\circ}) - \cos(\theta - 30^{\circ})]$$

$$= V_{I} I_{L} (\cos\theta \cos 30^{\circ} - \sin\theta \sin 30^{\circ})$$

$$-\cos\theta \cos 30^{\circ} - \sin\theta \sin 30^{\circ})$$
 (12.68)

$$= -V_{L} I_{L} 2 \sin 30^{\circ} \sin\theta$$

$$P_{2} - P_{1} = V_{L} I_{L} \sin\theta$$

since $2 \sin 30^\circ = 1$. Comparing Eq. (12.68) with Eq. (12.51) shows that the difference of the wattmeter readings is proportional to the total reactive power, or

$$Q_T = \sqrt{3}(P_2 - P_1)$$

(12.69)

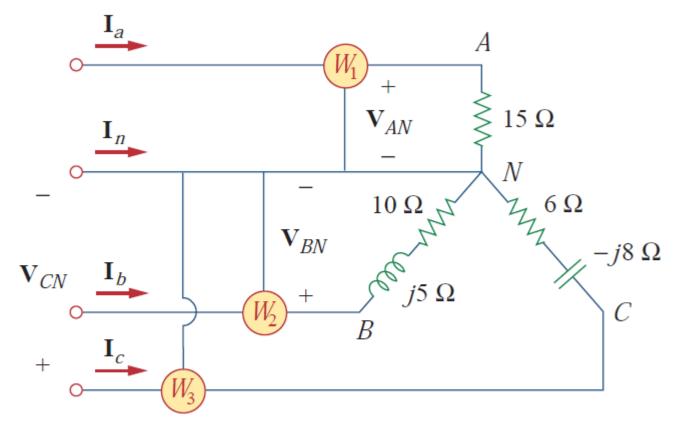


Figure 12.36 For Example 12.13.

RESIDENTIAL WIRING IN USA

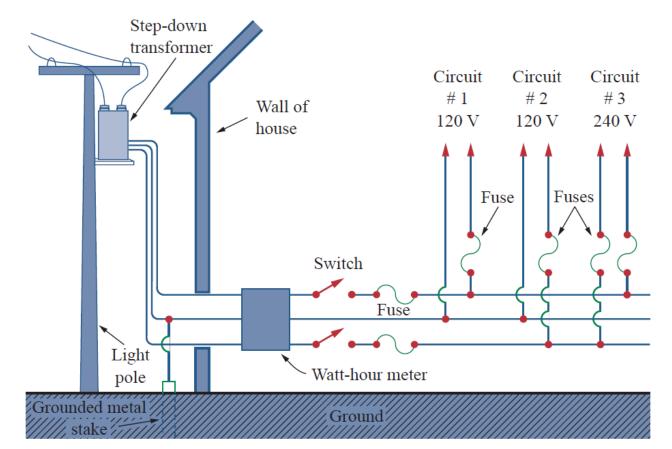


Figure 12.37 A 120/240 household power system.

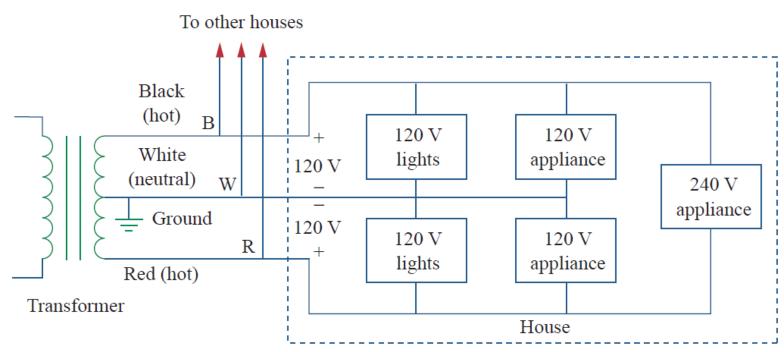


Figure 12.38

Single-phase three-wire residential wiring.